Lithographic Objective having a First Lens Group including only Lenses having a Positive Refractive Power

Field of the Invention

The invention relates to a projection objective for microlithography which has at least two lens groups which have positive refractive power.

Background of the Invention

United States Patent 5,990,926 discloses a projection lens system for use in microlithography and this lens system has three bellied regions, that is, three lens groups of positive refractive power. The objective is viewed in the direction of the propagation of the light. Here, the first lens group includes only positive lenses and the wafer end numerical aperture is 0.6.

United States Patent 5,969,803 discloses a projection objective for use in microlithography and this lens system includes three positive lens groups. The numerical aperture again is 0.6 and the objective here is a purely spherical objective.

European patent 0,332,201 discloses an optical projection system for microlithography wherein, at the wafer end, the last two lenses have respective aspherical lens surfaces for improving imaging quality. The aspherical lens surfaces are arranged facing toward each other.

The projection systems known from the above European patent are provided for photolithography and correspondingly have a low number of lenses. The imaging quality attainable therewith does not meet the requirements which are imposed on projection systems for microlithography. Especially, the numerical aperture, which

can be made available by means of this objective, is only 0.45.

Summary of the Invention

It is an object of the invention to provide a projection objective for microlithography which has a high numerical aperture as well as excellent imaging qualities.

The projection objective of the invention includes: a first lens group of positive refractive power; a second lens group of negative refractive power; at least one additional lens group having positive refractive power and the one additional lens group having a diaphragm mounted therein; the first lens group including only lenses having positive refractive power; the one additional lens group having a number of lenses of positive refractive power arranged forward of the diaphragm; and, the number of lenses of positive refractive power of the first lens group being less than the number of lenses of positive refractive power of the one additional lens group arranged forward of the diaphragm.

A projection objective is provided which has an especially high numerical aperture while at the same time having a low structural length because of the following measures: a first lens group which is so configured that this lens group comprises only lenses of positive refractive power and the number of lenses of positive refractive power of the first lens group is less than the number of the positive lenses which are mounted forward of the diaphragm of the additional lens group of positive refractive power.

In the input region of the objective, an expansion of the input beam is avoided by providing the first lens group which has only lenses of positive refractive power. Because of this measure, this first lens group can be configured to be very slim,

that is, the lenses have a small diameter. In this way, less material is needed in the first lens group, on the one hand, and, on the other hand, the structural space, which is needed to accommodate this lens group, is reduced. This structural space can be used to increase the numerical aperture by providing additional positive lenses forward of the diaphragm.

For an especially slimly configured first lens group, it is possible to shift the Petzval correction into these follow-on lens groups of positive refractive power because of the structural space obtained with a slight enlargement of these follow-on lens groups of positive refractive power. An especially large contribution to the Petzval correction is supplied by the positive lens group in which the diaphragm is mounted in combination with the strong beam narrowing forward of this group via a strong negative refractive power.

Preferably, the diameter of the lenses of the first lens group is less than 1.3 times the object field.

It has been shown to be advantageous to provide at least one lens having an aspheric surface in the first lens group. This aspheric surface contributes to improving the imaging quality of the objective.

It has been shown to be advantageous to provide aspheric lens surfaces in the first lens group which deviate by more than 300 μm compared to the best fitting spherical lens surface. The arrangement of such an asphere on the object end lens surface of the first lens of the lens arrangement has been shown to be advantageous. These intense asphericities close behind the reticle are necessary and are especially effective in order to correct the field-dependent aberration. The extent of the asphericity is dependent upon the beam cross sections and on the

input aperture which is always less than the output aperture. Even though the deviation to the sphere is great, a simple asphere form generates the most favorable contribution to the total aberration correction. As a consequence of the simple asphere form, this asphere form remains nonetheless easy to manufacture.

Brief Description of the Drawings

The invention will now be described with reference to the drawings wherein:

FIG. 1 is a schematic showing the assembly of a projection exposure system;

FIG. 2 is a schematic side elevation view of a projection objective for 248 nm having a numerical aperture of 0.8;

FIG. 3 is a schematic side elevation view of a projection objective for 193 nm having a numerical aperture of 0.8; and,

FIG. 4 is a schematic side elevation view of another projection objective for 248 nm having a numerical aperture of 0.8.

Description of the Preferred Embodiments of the Invention

First, the configuration of a projection exposure system will be described with reference to FIG. 1.

The projection exposure system 1 includes an illuminating unit 3 and a projection objective 5. The projection objective 5 includes a lens arrangement 19 having an aperture diaphragm AP. An optical axis 7 is defined by the lens arrangement 19. Different lens arrangements are explained hereinafter with reference to FIGS. 2 and 3. A mask 9 is mounted between the illuminating unit 3 and the projection objective 5 and the mask is held in the beam path with the aid of a mask holder. Masks 9 used in microlithography have a micrometer-nanometer structure.

This structure is imaged on an image plane 13 by means of the projection objective 5 demagnified up to a factor of 10 (demagnified especially by a factor of 4). A substrate 15 or a wafer, which is positioned by a substrate holder 17, is held in the image plane 13.

The minimal structures, which can still be resolved, are dependent upon the wavelength λ of the light, which is used for the illumination, as well as on the image-end numerical aperture of the projection objective 5. The maximum achievable resolution of the projection exposure system 1 increases with a decreasing wavelength λ of the illuminating unit 3 and with an increasing image-end numerical aperture of the projection objective 5.

In FIG. 2, a projection objective for microlithography is shown. This objective includes six lens groups.

The first lens group includes three positive lenses L101 to L103, which are all biconvex. The last lens L103 is provided with an asphere on the image-end surface. A targeted correction of the coma in the region of the image field zone is possible via the aspheric surface provided forward of the first waist or narrowing. The aspheric lens surface has only a slight influence on the inclined spherical aberration in the tangential section and in the sagittal section. In contrast, the inclined sagittal aberration (especially in the region between the image field zone and the image field edge) can be corrected with the aspherical lens surface after the narrowing or waist.

The provision of a second aspherical lens surface is a valuable measure in order to counter, with an increased aperture, a reduction of the image quality based on coma.

The second lens group includes four lenses L104 to L107. The image-end mounted lens surface of this last lens L107 of the

second lens group includes an aspheric lens surface. By means of this aspheric lens surface, especially a correction of image aberrations in the region between the image field zone and the image field edge is possible. The aberrations of higher order, which become noticeable with the observation of sagittal sections, are corrected. This is an especially valuable contribution because these aberrations, which are apparent in the sagittal section, are especially difficult to correct.

The third lens group includes the lenses L108 to L111. This lens group has a positive refractive power. The last image-end disposed lens surface of the last lens of this group is aspheric. This asphere operates, on the one hand, advantageously on the coma and, on the other hand, this asphere operates in a correcting manner on the axial aberration and on the inclined spherical aberration. The correction of the aberration is especially possible because of the large beam diameter in the region of this aspheric surface.

The following lens group having the lenses L112 to L115 has a negative refractive power.

The lens group following the above has a positive refractive power and includes lenses L116 to L123. A diaphragm is mounted in this lens group and this diaphragm is provided after the lens L119 so that four lenses of positive refractive power are mounted forward of the diaphragm. The excellent correction of the aberrations of this objective is attributable primarily to the positive lenses forward of the diaphragm. These lenses have a large component focal length because of the large diameter thereof, whereby the field loading drops and an improved correction at a higher numerical aperture is possible. These positive lenses operate, inter alia, advantageously on the coma.

Furthermore, this lens group is characterized by a reduced number of lenses.

The sixth and last lens group includes the lenses L124 to L127. The precise data of the lenses are presented in Table 1. The image field is 8 x 26 mm. It is noted that this objective has a very significantly high numerical aperture and yet has only 27 lenses. The required space for this objective is 1000 mm. The precise lens data are presented in Table 1.

Table 1

Lenses	Radius		Thickness	Material	½ Lens Diameter	Refractive Index at 248 nm
0	infinite		20.9706	L710	61.246	0.999982
L101	1160.20105		13.5756	SIO2	66.130	1.508373
	-363.46168		0.7500	L710	66.788	0.999982
L102	256.92295		20.1184	SIO2	68.174	1.508373
	-429.93637		0.7500	L710	67.973	0.999982
L103	353.94471		15.3795	SIO2	66.245	1.508373
	-1064.34630	A	0.7500	L710	65.385	0.999982
L104	365.62225		10.0788	SIO2	62.164	1.508373
	150.28204		24.6344	L710	57.665	0.999982
L105	-160.21163		7.0000	SIO2	57.121	1.508373
	138.69010		27.4314	L710	57.066	0.999982
L106	-257.68200		7.0000	SIO2	57.709	1.508373
	280.52202		27.7747	L710	62.688	0.999982
L107	-122.86419		7.000	SIO2	64.152	1.508373
	-524.02005	A	21.2270	L710	75.975	0.999982
L108	-334.99360		27.7619	SIO2	88.903	1.508373
	-142.00372		0.7500	L710	92.514	0.999982
L109	-1079.51219		40.8554	SIO2	109.187	1.508373
	-172.00795		0.7500	L710	111.327	0.999982
L110	438.67858		43.4000	SIO2	122.583	1.508373

	-378.94602		0.7500	L710	122.708	0.999982
L111	162.47382		51.1885	SIO2	113.015	1.508373
	-5736.26278	A	0.7500	L710	110.873	0.999982
L112	165.15494		14.7530	SIO2	92.577	1.508373
	110.95539		37.6018	L710	79.631	0.999982
L113	-2352.60464		7.0000	SIO2	78.360	1.508373
	158.84317		34.9167	L710	71.086	0.999982
L114	-168.34448		7.0000	SIO2	70.590	1.508373
	245.44885		39.3735	L710	71.824	0.999982
L115	-113.75821		7.0000	SIO2	72.408	1.508373
	666.85880		23.5469	L710	88.173	0.999982
L116	-278.47485		16.7462	SIO2	90.415	1.508373
	-195.62311		0.75000	L710	95.097	0.999982
L117	1596621.30490		37.6629	SIO2	113.071	1.508373
	-223.02293		0.7500	L710	115.353	0.999982
L118	2651.21287		31.3744	SIO2	127.060	1.508373
	-371.06734		0.7500	L710	128.117	0.999982
L119	1313.12466		25.1961	SIO2	131.302	1.508373
	-666.16100		0.0		131.498	1.000000
	infinite		9.5632	L710	130.856	0.999982
Diaphragm			0.0		130.856	
L120	812.62806		22.4028	SIO2	132.498	1.508373
	-1458.91764		10.9629	L710	132.481	0.999982
L121	344.45037		42.1137	SIO2	130.307	1.508373
	-765.47811		20.1268	L710	129.380	0.999982
L122	-250.24553		7.000	SIO2	127.451	1.508373
	-632.30447		15.5964	L710	127.304	0.999982
L123	-398.61314		20.5840	SIO2	126.393	1.508373
	-242.62300		1.2010	L710	126.606	0.999982
L124	143.95358		37.1050	SIO2	103.455	1.508373
	419.96225		0.8946	L710	100.698	0.999982
L125	120.37736		30.9217	SIO2	85.039	1.508373
	263.87928		14.8885	L710	79.055	0.999982
L126	1886.79345		7.6305	SIO2	74.319	1.508373

	277.58693		3.7474	L710	65.935	0.999982
L127	144.27214		50.1938	SIO2	58.929	1.508373
	423.41846		15.0000	L710	32.250	0.999982
0'	infinite		0.0001	L710	13.602	* 0.999982

L710 is air at 950 mbar.

<u>Asphere L103</u>:

EX= 0

C1= $-0.10457918*10^{-6}$

C2= $0.37706931*10^{-11}$

C3= $0.61848526*10^{-16}$

C4= $-0.13820933*10^{-19}$

C5= $0.36532387*10^{-24}$

C6= $-0.11262277*10^{-28}$

<u>Asphere L107</u>:

EX= $0.4532178*10^{2}$

C1= $0.19386780*10^{-7}$

C2= $-0.22407622*10^{-11}$

C3= $-0.42016344*10^{-15}$

C4= $0.45154959*10^{-19}$

C5= $-0.19814724*10^{-23}$

C6= $-0.43279363*10^{-28}$

<u>Asphere L111</u>:

EX= 0

C1= $0.57428624*10^{-8}$

C2= $0.22697489*10^{-12}$

C3= $-0.71160755*10^{-18}$

C4= $-0.72410634*10^{-21}$

C5= $0.32264998*10^{-25}$

C6= $0.55715555*10^{-30}$

The aspheric surfaces are described by the equation:

$$P(h) = \frac{\delta \cdot h \cdot h}{1+\sqrt{1-(1-EX)\cdot\delta\cdot\delta\cdot h\cdot h}} + C_1 h^4 + \ldots + C_n h^{2n+2} \qquad \delta = 1/R$$

wherein: P is the arrow height as a function of the radius h (height to the optical axis 7) with the aspherical constants C_1 to C_n presented in Table 1; R is the apex radius and is given in the table.

In FIG. 3, a projection objective is shown for the

wavelength 193 nm and has a numerical aperture of 0.8. A field of 8 x 26 can be exposed by means of this objective. The required structural space of this objective is 1000 mm.

The first lens group includes only two positive lenses and both are biconvex. The first lens L201 of this lens group G1 is provided with an aspheric lens surface at the object end.

The second lens group G2 includes the lenses L203 to L205. The lens L203 is provided with an aspheric lens surface at the object end. Because of the two aspheric lens surfaces of the lenses L201 and L203, which are provided in the first and second lens groups (G1, G2), respectively, and are arranged so as to be close to the field, an excellent beam separation in the input region of the objective is obtained. The arrangement of the aspheric lens surfaces on the side, which faces to the object, affords the advantage that the lenses, which have an aspheric lens surface, lie with the spherical lens surface against a lens frame. In this way, an excellent contact engagement on the lens frame with the spherical lens surface can be more easily ensured.

The third lens group G3 includes the lenses L206 to L210. This lens group has a positive refractive power. The two lenses L208 and L209 have two surfaces greatly curved toward each other. The last lens L210 of this lens group includes, at the image end, an aspheric lens surface. An excellent coma correction can be carried out by means of this aspheric lens surface. Furthermore, a correction of the axial and inclined spherical aberrations is especially possible in this region because of the large beam diameters.

The fourth lens group includes lenses L211 to L214. This lens group overall has a negative refractive power. In the next and fifth lens group G5, which includes the lenses L215 to L220,

the diaphragm is mounted after the lens L217. This lens group includes three positive lenses and the last lens forward of the diaphragm is configured to be especially thick. The last lens group G6 includes the lenses L221 to L225 and the lens L224 is configured to be especially thick. An intense spherical overcorrection is obtained with this lens.

The precise lens data is presented in Table 2.

Table 2

Lenses	Radius		Thickness	Material	½ Lens Diameter	Refractive Index at 193 nm
0	infinite		32.7500	L710	61.249	0.999982
L201	469.70813	A	14.5480	SIO2	62.591	1.560289
	-20081.10295		5.1612	HE	63.071	0.999712
L202	354.86345		18.8041	SIO2	63.983	1.560289
	-334.15750		9.4004	HE	63.889	0.999712
L203	381.44025	A	28.0599	SIO2	61.107	1.560289
	140.16853		27.1615	HE	55.898	0.999712
L204	-149.89590		23.2652	SIO2	55.910	1.560289
	229.41466		33.1065	HE	62.024	0.999712
L205	-105.40274		7.0000	SIO2	63.462	1.560289
	-336.55620		16.9549	HE	74.238	0.999712
L206	-165.03805		10.7419	SIO2	78.416	1.560289
	-147.21753		0.7575	HE	82.164	0.999712
L207	-314.39712		27.7710	SIO2	90.707	1.560289
	-145.41305		0.7500	HE	94.176	0.999712
L208	-50326.68803		38.7705	SIO2	107.592	1.560289
	-211.33124		0.7500	HE	109.537	0.999712
L209	184.32395		41.8364	SIO2	112.438	1.560289
	1282.45923		0.7500	HE	110.470	0.999712
L210	153.97703		35.8150	SIO2	99.821	1.560289

	538.04124	A	8.4636	HE	95.507	0.999712
L211	180.72102		7.8641	SIO2	82.558	1.560289
	116.94830		38.5761	HE	73.768	0.999712
L212	-292.06054		7.0000	SIO2	71.989	1.560289
	121.89815		26.8278	HE	65.096	0.999712
L213	-416.86096		7.0000	SIO2	65.191	1.560289
	320.06306		34.0097	HE	66.681	0.999712
L214	-106.74033		7.1599	SIO2	67.439	1.560289
	842.66128		12.4130	HE	82.767	0.999712
L215	-531.44217		35.2270	SIO2	84.311	1.560289
	-173.85357		0.7500	HE	93.111	0.999712
L216	5293.05144		34.6817	SIO2	109.462	1.560289
	-359.30358		5.8421	HE	114.271	0.999712
L217	1423.10335		73.8658	SIO2	123.709	1.560289
	-302.64507		11.7059	HE	130.054	0.999712
	infinite		-4.1059	HE	129.751	0.999712
	infinite		0.0000		129.751	
L218	644.68375		29.3314	SIO2	130.947	1.560289
	-1224.04524		0.7500	HE	130.998	0.999712
L219	324.02485		28.7950	SIO2	129.211	1.560289
	1275.35626		44.6599	HE	127.668	0.999712
L220	-246.29714		25.7695	SIO2	126.964	1.560289
	-260.21284		0.7500	HE	129.065	0.999712
L221	265.62632		25.9894	SIO2	115.965	1.560289
	689.74229		1.8638	HE	113.297	0.999712
L222	148.08236		25.7315	SIO2	100.768	1.560289
	256.32650		14.8743	HE	97.685	0.999712
L223	130.15491		28.8792	SIO2	81.739	1.560289
	554.81058		6.6463	HE	77.855	0.999712
L224	infinite		67.6214	CAF2HL	76.291	1.501436
	infinite		0.9000	HE	33.437	0.999712
L225	infinite		4.0000	SIO2	32.220	1.560289
0'	infinite			L710	29.816	0.999982

L710 is air at 950 mbar.

Asphere L201:

EX= 0

C1= $0.98184588*10^{-7}$

C2= $-0.34154428*10^{-11}$

C3= $0.15764865*10^{-15}$

C4= $0.22232520*10^{-19}$

C5= $-0.79813714*10^{-23}$

C6= $0.71685766*10^{-27}$

Asphere L203:

EX= 0

C1= $0.26561042*10^{-7}$

C2= $0.78262804*10^{-12}$

C3= $-0.24383904*10^{-15}$

C4= $-0.24860738*10^{-19}$

C5= $0.820928858*10^{-23}$

C6= $-0.85904366*10^{-27}$

Asphere L210:

EX= 0

C1= $0.20181058*10^{-7}$

C2= $-0.73832637*10^{-12}$

C3= $0.32441071*10^{-17}$

C4= $-0.10806428*10^{-21}$

C5= $-0.48624119*10^{-25}$

C6= $0.10718490*10^{-2}$

In FIG. 4, a further lens arrangement 19 is shown which is designed for the wavelength 248 nm. This lens arrangement includes 25 lenses which can be subdivided into six lens groups. The structural length of this lens arrangement from object plane 0 to image plane 0' is 1000 mm. The numerical aperture of this lens arrangement is 0.8 of the image end.

The first lens group G1 includes two positive, biconvex lenses L301 and L302. The lens L301 is provided with an aspheric lens surface at the object end.

The second lens group G2 has negative refractive power and includes the lenses L303 to L305. The lens L303 is provided with an aspherical lens surface at the object side. An excellent correction of field aberrations is possible with these two aspheric lens surfaces of the lenses L301 and L303. Furthermore,

a clear beam separation is achieved because of these aspheres mounted close to the field.

The third lens group G3 includes the lenses L306 to L310 and has a positive refractive power. The lens L310 is provided with an aspheric lens surface at the image end. By means of this aspheric lens surface, an especially good correction of the coma and the axial and inclined spherical aberrations is possible. An arbitrated correction between axial and inclined spherical aberrations is especially possible because of the large beam diameters which are, however, significantly less than the clear lens diameters.

The fourth lens group G4 comprises the lenses L311 to L314 and has a negative refractive power.

The fifth lens group G5 includes the lenses L315 to L320 and has an overall positive refractive power. A diaphragm AP is mounted after the lens L317. By providing the clear air space between lens L317 and lens L318, it is possible to arrange a slide diaphragm between these two lenses.

The sixth lens group G6 includes the lenses L321 to L325. This lens group likewise has a positive refractive power. The meniscus lenses L321 to L323 are curved on both sides toward the object. This lens group includes only concave lenses which effect a field-independent, intense spherical overcorrection. For objectives having a high aperture, a correction of the spherical aberration also of higher order is possible by means of such conversion lenses.

This objective is especially well corrected especially because of the use of the aspheric lens surfaces as well as because of the specific arrangement of the number of positive lenses of the first lens group and because of the higher number

of positive lenses forward of the diaphragm. The deviation from the wavefront of an ideal spherical wave is a maximum of 5.0 mλ for a wavelength of 248 nm.

Preferably, the aspheric lens surfaces are arranged on the forward lens surface whereby the corresponding lens lies with its spherical lens surface on the frame surface. In this way, these aspherical lenses can be framed with standard frames. The precise lens data are presented in Table 3.

Table 3

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SURFACE	RADII		THICKNESSES	GLASSES	REFRACTIVE INDEX 248.338 nm	½ FREE DIAMETER
0	infinite		32.750000000	L710	0.99998200	54.410
1	480.223886444	AS	16.335451604	SIO2	1.50839641	62.519
2	-1314.056977504		2.406701682	L710	0.99998200	63.128
3	329.047567482		20.084334424	SIO2	1.50839641	63.870
4	-305.091682732		4.977873027	L710	0.99998200	63.737
5	383.800850809	AS	34.498893572	SIO2	1.50839641	61.345
6	132.468446407		27.572735356	L710	0.99998200	54.949
7	-146.238861297		7.000000000	SIO2	1.50839641	54.908
8	202.067070373		26.902804948	L710	0.99998200	58.294
9	-124.60415239		7.000000000	SIO2	1.50839641	59.529
10	-9484.579900199		32.328722869	L710	0.99998200	69.147
11	-199.920035154		13.239699068	SIO2	1.50839641	80.852
12	-156.061108055		0.750000376	L710	0.99998200	84.387
13	-647.599685325		32.765465982	SIO2	1.50839641	96.077
14	-169.327287667		0.750000000	L710	0.99998200	99.492
15	54987.154632328		43.791248851	SIO2	1.50839641	110.237
16	-198.179168899		0.750000000	L710	0.99998200	112.094
17	179.965671297		37.961498762	SIO2	1.50839641	110.618
18	730.008903751		0.750000000	L710	0.99998200	108.526
19	155.802150060		40.190627192	SIO2	1.50839641	99.471

20	525.570694901	AS	3.398727679	L710	0.99998200	93.056
21	210.625893853		10.671567855	SIO2	1.50839641	85.361
22	118.365024068		39.388505884	L710	0.99998200	74.596
23	-290.993996128		7.000000000	SIO2	1.50839641	72.941
24	153.643732808		24.440280468	L710	0.99998200	67.256
25	-364.763623225		7.000000000	SIO2	1.50839641	67.177
26	201.419421908		40.566258495	L710	0.99998200	68.276
27	-109.336657265		7.000000000	SIO2	1.50839641	69.319
28	1061.293067334		13.765515688	L710	0.99998200	84.656
29	-569.739152405		43.187833722	SIO2	1.50839641	87.749
30	-187.461049756		0.750000000	L710	0.99998200	99.718
31	1880.153525684		40.009394091	SIO2	1.50839641	117.515
32	-286.975850149		0.750000000	L710	0.99998200	120.535
33	1960.535354230		35.788625356	SIO2	1.50839641	127.909
34	-378.322213808		11.705900000	L710	0.99998200	129.065
35	infinite		-4.105900000	L710	0.99998200	129.546
36	665.988216308		27.299895961	SIO2	1.50839641	130.708
37	-1514.956732781		0.750000000	L710	0.99998200	130.863
38	392.166724592		35.529695156	SIO2	1.50839641	130.369
39	-2215.367253951		37.377386813	L710	0.99998200	129.155
40	-235.632993037		38.989537996	SIO2	1.50839641	128.458
41	-252.020337993		0.835229633	L710	0.99998200	131.819
42	269.631401556		32.688617719	SIO2	1.50839641	118.998
43	1450.501345093		0.750000001	L710	0.99998200	116.187
44	138.077824305		29.652384517	SIO2	1.50839641	100.161
45	255.416969175		2.589243681	L710	0.99998200	96.793
46	139.090220366		30.752909421	SIO2	1.50839641	86.930
47	560.532964454		8.142484947	L710	0.99998200	82.293
48	infinite		73.619847203	SIO2	1.50839641	79.524
49	infinite		0.900000000	L710	0.99998200	33.378
50	infinite		4.000000000	SIO2	1.50839641	32.173
51	infinite		12.000000000	L710	0.99998200	29.666
52	infinite					13.603

L710 is air at 950 mbar.

ASPHERIC CONSTANTS

SURFACE NO.	1		
EX	0.0000	C1	9.53339646e-008
C2	-3.34404782e-012	C3	1.96004118e-016
C4	8.21742864e-021	C5	-5.28631864e-024
C6	4.96925973e-028	C7	0.00000000e+000
C8	0.00000000e+000	C9	0.00000000e+000
SURFACE NO.	5		
EX	0.0000		
C1	2.89631842e-008	C2	7.74237590e-013
C3	-2.72916513e-016	C4	-8.20523716e-021
C5	4.42916563e-024	C6	-5.10235191e-028
C7	0.00000000e+000	C8	0.00000000e+000
C9	0.00000000e+000		
SURFACE NO.	20		

Ex	0.0000
C1	1.99502967e-008
C2	-7.64732709e-013
C3	3.50640997e-018
C4	-2.76255251e-022
C5	-3.64439666e-026
C6	5.10177997e-031
C7	0.00000000e+000

It is understood that the foregoing description is that of the preferred embodiments of the invention and that various changes and modifications may be made thereto without departing from the spirit and scope of the invention as defined in the appended claims.